DALLARA F300

FORMULA 3/2000 USER MANUAL

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GENERAL DIMENSIONS AND SUPPLIERS

| Wheelbase | 2678mr |
|-------------------------|-----------------------------------------------------------------------------------------------------------------|
| Front Track | 1500mn |
| Rear Track | 1430mn |
| Overall height | 915 mm (from ground to top of roll hop |
| Overall width | 1750 mm (wide front suspension |
| Overall length | 4060 mm (front endplate to rearmost edge of rear wing |
| Weight | 540 Kg (including driver and ballast) |
| Front suspension | push-rod monodamper |
| Rear suspension | push-rod twin damper |
| Chassis | Carbon and KEVLAR™ sandwich with AL / NOMEX™ h/comb |
| Bodywork | Glass fibre prepreg with NOMEX honeycomb |
| Composites | HEXCEL-HERCULES |
| Castings | AGUSTA/FLABO |
| Gearbox | DALLARA casing, five ratios and reverse gear |
| Gears and differential | HEWLAND |
| Springs | EIBACH 36 mm ID |
| Dampers | KONI 2812-140 (bump and rebound adjustable) |
| Fuel cell | PREMIER - FT3 |
| Extinguisher system | SPA design (electrical operated) |
| Steering wheel | OMP – 270 mm OD |
| Steering release system | SPA design |
| Coolers | BEHR |
| Filters | FIAAM |
| Rims | SPEEDLINE 9" front – 10.5" rear |
| Brake system | BREMBO |
| Battery | FIAMM |
| Seat belt | TRW-SABELT |
| Installed engines | Fiat, Alfa, BMW Novamotor Honda Mugen Opel Spiess Renault Sodemo Toyota Tom's Mitsubishi HKS VW Bertil's (USA). |

SET-UP

TIRE INFORMATION

Tire dimensions depend on tyre pressure, rim width and camber angle.

The stiffness values are based on the recommended inflating pressure (hot tyres).

| | Avan | Bridgestone | Michelin | Pirelli | Yokohama |
|----------------------------|------------|-------------|-----------|------------|-----------|
| FRONT TIRE | Avon | 180/550-13 | 20/54-13 | 200/530-13 | 180/50-13 |
| Specification | 180/550-13 | | 272.3 | 266.3 | 278.0 |
| Free radius (mm) | 277.5 | 277.2 | | 261.5 | 273.2 |
| Loaded radius (mm) | 272 | 271.5 | 267.8 | | 17.0 |
| Vertical stiffness (Kg/mm) | 21.0 | 14.4 | 20.7 | 17.1 | |
| Hot tire pressure (bar) | 1.5 | 1.5 | 1.55 | 1.5 | 1.6 |
| REAR TIRE | | | 104/57 40 | 250/575-13 | 240/45-13 |
| Specification | 250/570-13 | 240/570-13 | 24/57-13 | | 288.0 |
| Free radius (mm) | 287.0 | 286.5 | 289.1 | 289.4 | |
| | 281.3 | 279.0 | 284.0 | 282.0 | 281.0 |
| Loaded radius (mm) | | 16.7 | 21.8 | 17.2 | 17.8 |
| Vertical stiffness (Kg/mm) | 22.8 | | 1.6 | 1.55 | 1.55 |
| Hot tire pressure (bar) | 1.65 | 1.5 | 11.0 | 1 | |

SUGGESTED SETUP

The set-ups consider the complete car with the driver seated, ready to race. The front anti roll setting pre-load is 'double stiffness' pre-load, for details look at the FARB pages.

| | Avan | Bridge | Michelin | Pirelli | Yokohama |
|------------------------------|---------|---------|----------|---------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| FRONT | Avon | 15 | 15 | _ -15 | 15 |
| Ride height (mm) | 15 | | 3°45' | 4° | 3°15' |
| Camber (deg) | 2°45' | 3°15′ | 20' OUT | 20' OUT | 20.OUT |
| Toe (deg) (total two wheels) | 20' OUT | 10' OUT | | 800 | 700 |
| Springs (lb/in) | 800 | 700 | 800 | 5 | 5 |
| Vertical Pre-load (mm) | 8 | 6 | 8 | 5 | |
| | 6 | 6 | 6 | 6 | 6 |
| Solid spacer (mm) | | 682.5 | 689.5 | 689.5 | 682.5 |
| Push rod length (mm) | 682.5 | STD | STD | STD | STD |
| Roll centre setting | STD | <<>><< | <<>>>< | <<>>>< | <<>>>< |
| Roll bar setting | <<>><< | | 9 | 9 | 0 |
| Roll pre-load (notches) | 9 | 9 | 9 | | A STATE OF THE STA |
| REAR | | | | 34 | 34 |
| Ride height (mm) | 34 | 34 | 34 | 3°15' | 2°45' |
| Camber (deg) | 2°00' | 2°15' | 3°30' | 0 | 10'IN |
| Toe (deg) (total two wheels) | 10' IN | 20' IN | 0 | | 800 |
| Springs (lb/in) | 900 | 800 | 900 | 900 | |
| Pre-load (mm) | 0 | 0 | 0 | 0 | 0 |
| | | | 570 | 572 | 572 |
| Push rod length (mm) | 572 | 572 | 572 | STD | STD |
| Roll centre setting | STD | STD | STD | | 24 OD |
| Roll bar | 21 OD | 24 OD | 24 OD | 24 OD | 60/80#4 |
| Differential setting | 60/80#4 | 60/80#6 | 60/80#4 | 60/80#6 | 100/00#4 |

SETUP ADJUSTMENT

EFFECTS ON ADJUSTMENTS ON THE SET-UP

| Positive change in: | means: |
|---------------------|--------------------------------|
| Height | car rises |
| Toe | toe-out |
| Camber | upper part of rim outward |
| Castor | lower part of rim points ahead |

ADJUSTMENTS

| | | FI Ph. 6.3 LAW | |
|----------------------------------------------------------------|---------------------|---------------------|------------------------|
| 5.10.15.05.45.11.05 | | FRONT | REAR |
| PUSHROD ADJUSTE | ER | | |
| | Height change | 4.30mm | 6.52mm |
| +1TURN | Camber change (deg) | 2' | 14' |
| | Thread step | M1.25R+24/"L=2.31mm | M1.25R+24/"L=2.31mm |
| TOE ADJUSTER (PE | R | | |
| WHEEL) | | | |
| +1TURN | toe change (deg) | 36' | 1°25' |
| | thread step | 24/" | M1.25R+24/"L=2.31mm |
| CAMBER SPACER | +1mm | 17' | 15' |
| | toe variation | | 0.5mm = 18' |
| CASTOR ADJUSTER | | | 20° brakecaliper=14.5° |
| | Castor change (deg) | 26' | -38' |
| | thread step | 24/" | 20/" |
| +1TURN | height change (mm) | -0.8 | -0.2 |
| | camber change (deg) | -7' | 4' |
| | toe change (deg) | 2' | -4' |
| SPRING PLATFORM | | | |
| +1TURN | thread step (mm) | 2 | 2 |
| TIOITH | height change (mm) | 1.78 | 2.42 |
| WHEEL (SPRING PATI | | 0.91 | 1.21 |
| WHEEL/SPRING RATIO (vertical) WHEEL/BELLEVILLE RATIO (lateral) | | | 1.21 |
| | | 1.56 | |
| WHEEL/DROP LINK RA | | | 1.77 |
| ROLL CENTRE HEIGH | | Tyre dependent | Tyre dependent |

Available front camber spacers: 1.0, 1.5 and 2.0 mm. For the rear are available 0.8, 1.0, 1.2, 1.5 and 2.0mm. Combine these to make fine adjustments.

Front and rear wheel to spring, front wheel to Belleville and rear wheel to drop link motion ratios may be considered as constant for all the wheel motion.

FRONT SUSPENSION

VERTICAL or SPRING PRELOAD

In a non pre-load condition, as long as the damper is not fully extended, turning the platform C raises the ride height and lowers slightly the pressure inside the damper. When the damper gets fully extended, turning-on the platform C puts vertical spring pre-load on the car. We advise though, not to proceed this way, because some dampers (including Koni) should not be used fully extended. Therefore we advise to use the droop-stop 'A'.

Remind that there is some pre-load in each damper. With a Koni damper this pre-load is about 30kg.

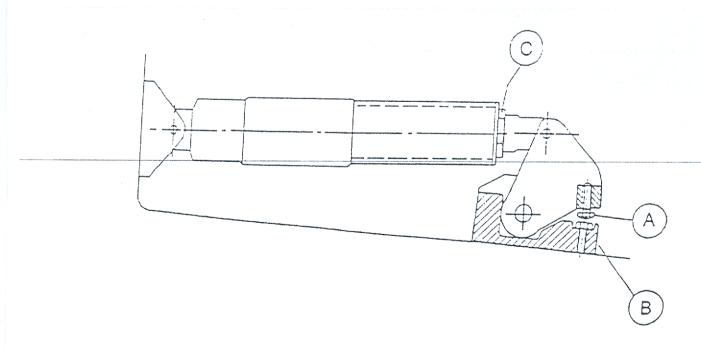
This pre-load depends on damper type, settings and internal gas pressure.

Pre-load is the force that has to be applied on the spring to start to modify its length with respect to the static value. To set the on car pre-load, put the car with the driver seated on the set-up floor. Unscrew the droop-stop A to contact the opposite bolt B. Now turn platform C to set the pre-load. As the platform thread step is 2 mm, the pre-load $P = Ks \times t \times 2$ P = pre-load in kg

Ks = spring stiffness in kg/mm (spring stiffness in Lb/in) / 56 = spring stiffness in kg/mm T = number of platform C turns 2 = mm / turn (for Koni)

SETTING THE 'ON CAR PRE-LOAD'

Mount the damper-spring combination with the platform C just in contact with the spring. Mount damper-spring combination on the car and put the car with the driver seated on the set-up floor. Make the car bounce a few times to settle down. Screw the droop-stop A into the rocker, away from touching bolt B. Adjust ride height with the pushrod adjusters to the desired setting. Bring droop-stop A in contact with bolt B. Turn platform C until desired pre-load force is achieved. (P = Ks x tTx 2)



FRONT ANTI ROLL AND PRE-LOAD

There are 3 different ways of setting the front anti-roll Belleville washers.

1) Mount a stack configuration and turn the platforms just in contact with the stack. This way there is no pre-load on the stack and the roll stiffness is the nominal stack stiffness.

For example: the configuration <<>><< gives 761kg/mm stiffness.

2) When both platforms get turned on a few notches the system is preloaded. The roll stiffness under this pre-load is double the nominal stiffness. When the rocker passes the pre-load the stiffness gets back to the nominal.

For example: >><<>> + 5 notches is for 0.5mm of lateral movement 761x2=1522kg/mm stiff.

3) When both platforms get turned on a few notches and locked up with the two extra locknuts the system is infinite stiff, this means there is no lateral movement as long as the force doesn't overcome the pre-load. Once the pre-load passed, the stiffness gets back to nominal.

Both pre-load settings (2 and 3) generally help for sharper turn-in.

- Soft no pre-load settings (1) can make the tyres last longer and make the car easier to
- Over the pre-load, the stiffness gets back to the nominal stiffness. The driver may prefer some pre-load in certain conditions (turn-in...) and wish to overcome the pre-load in some other conditions (mid corner, curbs...). Set accurately the transition point of 'preload / no pre-load' since the consequently stiffness variation is sudden and reflects immediately on the cars' balance and behaviour.
- You can combine different stacks in series to obtain a progressive load / displacement characteristic. Total length of the combined stack should never be more than 28mm.

-The clearance between the platform and the rocker (B) should not be more than 6.5mm when platform just touches the Belleville stack, with no pre-load.

-For any Belleville stack, in running condition, rocker lateral displacement and the chosen pre-load must never reach the "Maximum Deflection" (see Table below), to avoid a sudden lateral locking of the rocker.

BELLEVILLE STACK CONFIGURATIONS (Belleville thickness 2.0mm)

| Stack configuration | Nominal stiffness kg/mm | Stack length mm | Maximum deflection mm | | Maximum notches |
|---------------------|-------------------------------|-----------------------|-----------------------------|---------------|--------------------|
| <<<>>>> | 2504 | 17.50 | 1.12 | → | 8 |
| <<<>>> | 1796 | 13.50 | 1.12 | respect | 8 |
| <<<>>> | 1197 | 20.25 | 1.69 | maximum | 12 |
| <<>>>< | 761 | 14.25 | 1.69 | notches | 12 |
| <<>>>< | 571 | 19.00 | 2.25 | when using | 17 |
| <<>><<> | 457 | 23.75 | 2.81 | pre-load | 22 |
| | 362 | 8.25 | 1.69 | configu- | 14 |
| <>< | 272 | 11.00 | 2.25 | rations | 17 |
| <><> | 218 | 13.75 | 2.81 | \rightarrow | 22 |
| <><>< | 181 | 16.50 | 3.37 | | 26 |
| <><><> | 155 | 19.25 | 3.93 | | 28 |

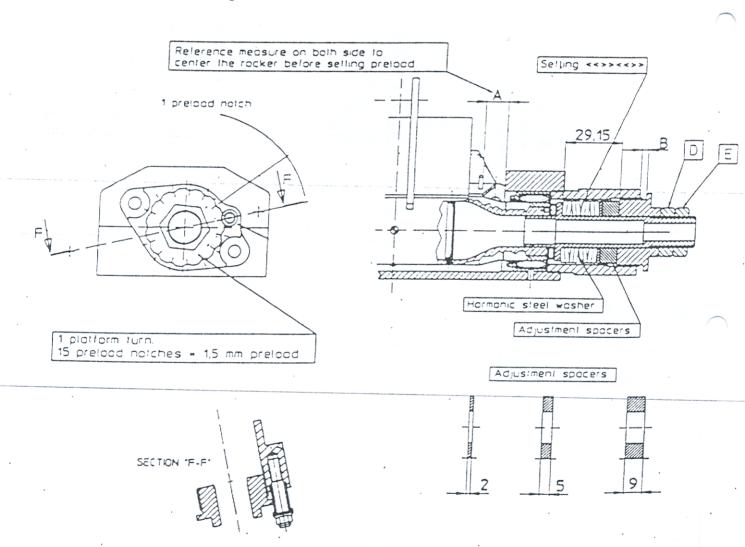
SETTING THE PRE-LOAD

DOUBLE STIFFNESS PRE-LOAD

- Mount the stack you want to use and turn the platform until contact with the Belleville stack
- Adjust by turning the platforms until distance A is the same on both sides
- Check distance B to be less than 6.5mm, if more, replace adjustment spacer
- Mark this platform position as the "zero pre-load" notch
- Turn both left and right platforms the amount of notches to set the desired pre-load. One turn of platform is 15 notches corresponding to 1.5mm displacement (1 notch = 0.1mm)

INFINITE STIFFNESS PRE-LOAD

- Set the pre-load as described for the double stiffness procedure here above
- Mount nut D in contact with the platform
- Tighten counter nut E against nut D

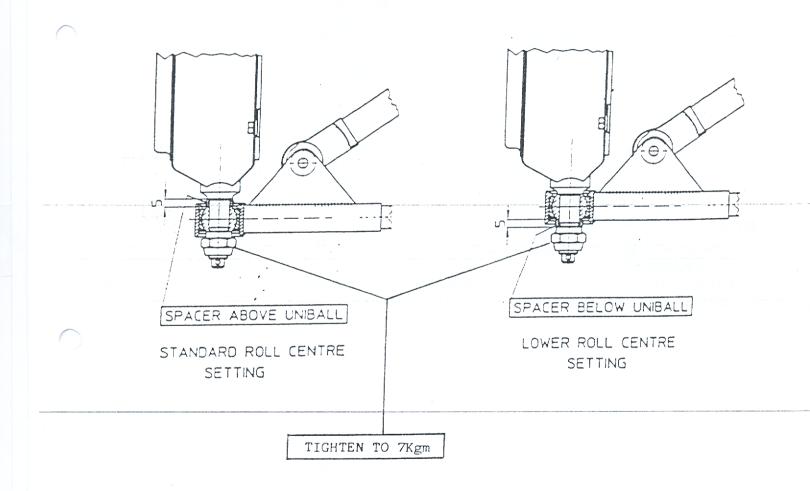


FRONT ROLL CENTER

Moving the spacer underneath or above the lower wishbone spherical joint changes the height of the front roll centre. When choosing "low roll centre" configuration, push-rod length has to be shortened by 1.4 register turns (8 faces of the adjuster) to keep the car at the same ride height.

When adjusting the roll centre height, there will also be a slight change in camber gain in function of vertical wheel travel.

| OPTION | Roll centre height | Camber change |
|--------|--------------------|-----------------------|
| | static ride height | for 10mm wheel travel |
| Std | X | 5' |
| Low | -12.5 mm | 3' |



STEERING ASSEMBLY

| Pinion primitive diameter | 15.71 mm | |
|---------------------------|---------------------------|--|
| Static steering ratio | 12.6 steering wheel/wheel | |
| Ackermann [%] | 28.5 | |

MEASURING CASTOR

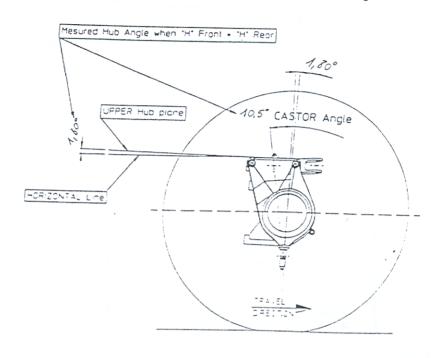
FRONT

When the car is flat (front ride height equals rear) and the front upright inclination is 1.80°, castor ang is 10.5°.

With different front to rear ride heights, castor angle changes because of the pitch angle of the ca For instance, with 15 mm front and 40mm rear ride height, measured at wheel axis, (wheelbase is 267 mm) the pitch angle is 0.53° as:

Pitch angle $(40-15)/2678 = 1 / \tan 0.53^{\circ}$

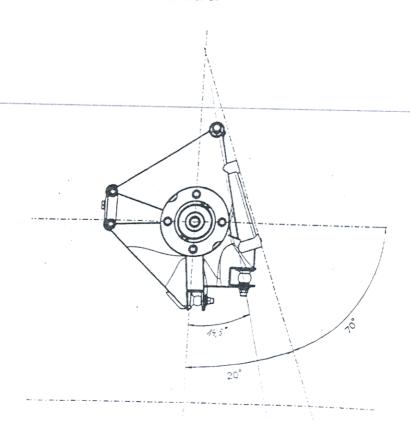
castor angle: 10.5° - 0.53° = 9.97°



REAR

The rear wheel castor (not relevant because the wheel is not steered) can be checked using the brake-

When the car is flat (front ride height equals rear) and the measured angle is 20° the castor is 14.5°. The pitch angle must be added because the castor is rearward.

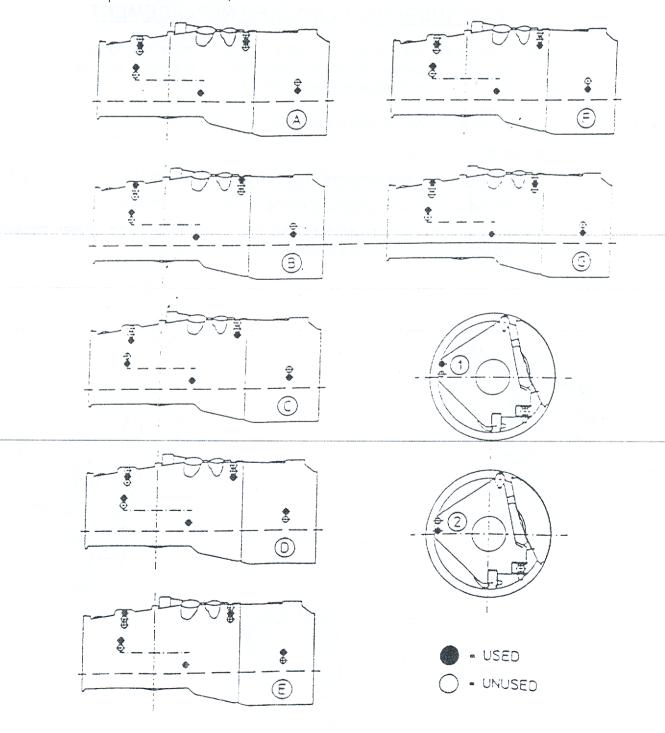


REAR SUSPENSION

REAR SUSPENSION ROLL CENTER AND ANTISQUAT SETTING

| OPTION | Roll centre height | Camber change | Antisquat |
|--------------|--------------------|-----------------------|-----------|
| 0. 1.0.1 | static ride height | for 10mm wheel travel | % |
| A-1 | std | 21' | 48 |
| B-2* | -15 | 17' | 48 |
| C-1 | +15 | 25' | 48 |
| D-1* | std | 21' | 60 |
| D-1* E-2* | -15 | 17' | 60 |
| F-1 | +5 | 22' | 30 |
| G-2 | -10 | 18' | 30 |

Option **D-1** and **E-2** alter caster angle. To obtain std value **shorten by 2 turns** the 'castor' uniball. Option **B-2** needs special bracket for front top mounting (available at Dallara)



Dallara Automobili

REAR ANTIROLL BAR STIFFNESS

F300 has a rear antiroll bar with two 75mm long adjustable blades.

40mm diameter ARB is the stiffest available, this can be milt down to any softer ARB.

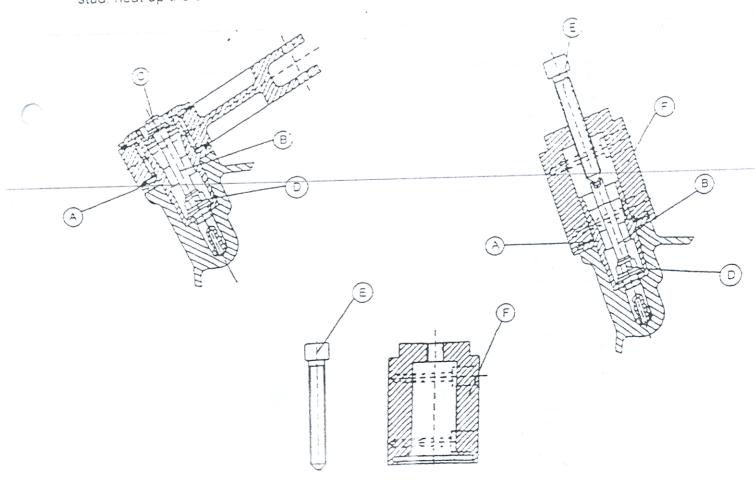
The two digits in this table represent the blade positions: 1=full soft, 5=full hard. Stiffness in kg/mm.

| | | | | 3-5 | 4-5 | 5-5 |
|-----------|------|-------|-------|-------|-------|-------|
| OD | 1-1 | 1-5 | 2-5 | | 27.0 | 27.6 |
| 14 mm | 22.6 | 24.8 | 25.1 | 25.9 | 44.0 | 45.5 |
| 16 mm | 33.4 | 38.6 | 39.2 | 41.2 | 79.5 | 84.6 |
| 19 mm | 50.6 | 63.3 | 65.1 | 70.9 | | 118.6 |
| | 61.1 | 80.7 | 83.6 | 93.4 | 108.9 | 177.9 |
| 21 mm | 73.8 | 104.3 | 109.2 | 126.7 | 156.8 | |
| 24 mm STD | 85.1 | 128.6 | 136.1 | 164.3 | 218.9 | 262.2 |
| 28 mm | 00.1 | 120.0 | | | | |

REAR SUSPENSION ROCKER REPLACEMENT

The rear rocker spins around a steel pivot 'A' fitted onto the gearbox casing by stud B, fixed with LOCTITE 242. The following procedure shows the disassembly of the rocker and the pivot A. Contact DALLARA customers' service to get the tools E and F.

- Unscrew nut C. The tightening torque to fit it back is 3.5 Kgm;
- Take off the top cap and the rocker;
- Unscrew nut D with a long 14mm tubular dowel. The tightening torque to fit it back is 5.5 Kgm;
- Fit extractor F around the pivot's outer flange, screwing in bolt E, and remove the pivot
- Remove stud-B with the proper tool. The stud-is-fitted with Loctite in its insert.—When removing the stud, heat up the stud's thread to break the Loctite with a heatgun up to 140 C°.



RIDE HEIGHT CHECK AND REFERENCES

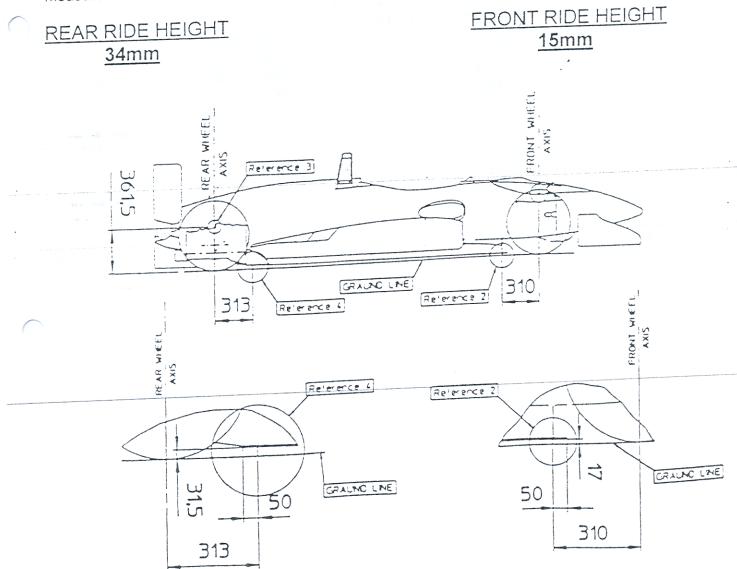
Ride height is fundamental for setting and changing the aerodynamic performance of the car. It might be difficult to measure it directly, so we provide alternative references. The example shows front ride height 15mm and rear 34mm (at wheel axis). With 2678mm wheelbase, pitch angle is 0.40°. Calculation: $(34 - 15) / 2678 = inv. tan x \rightarrow x = 0.40°$ (The two round platforms on top of the tub to measure front ride height at front axis are 50mm behind the axis when using the long wheelbase front suspension)

Measuring front ride height:

A flat surface (skid) about 310 mm behind the wheel axis and 50 mm behind the skid leading edge. You can measure its distance from ground as 17 - (tan0.40°x310)=15mm

Measuring rear ride height:

Two machined areas, at 327.5 mm from car bottom, on the gearbox at wheel axle line. You can measure their distance from the ground as 361.5 - 327.5 = 34mm height. Under the flat bottom, 50mm ahead of the start of the diffuser and 313mm ahead of the rear wheel axis, you can measure and calculate the floor distance from the ground as following: measured 32mm + (tan 0.40° x 313) = 34mm



POWER FLOW DIFFERENTIAL

WORKING PRINCIPLE AND SETUP

This differential ("diffs") is designed with versatility as its major asset. Many parameters will lead you to the required setting. A car with good grip and low power may require a completely different arrangement than that for a high power/low grip car.

The working principles of powerflow differentials:

Ten friction plates within the diff, six connected to the side gears, four to the diff casing, control the amount of differential action available. The amount of limited slip depends only on the frictional resistance between these ten plates.

Four factors contribute in defining this frictional resistance (see figure next page):

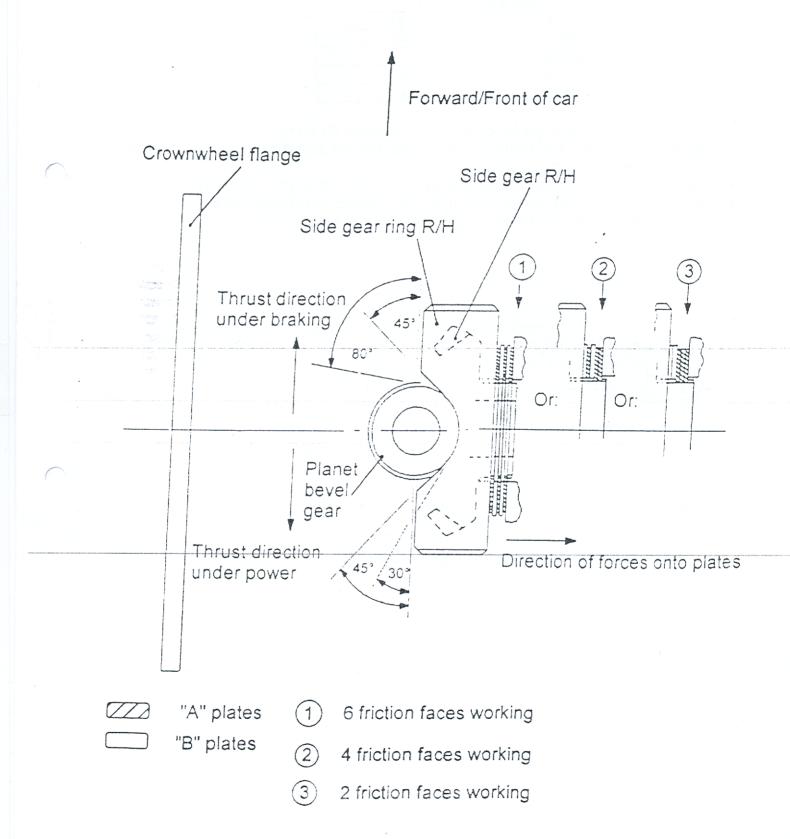
- 1. The bevel gears thrust apart as soon as the car moves. This is a feature of bevel gears and is not adjustable.
- 2. The ramp angle on the side gear ring influences the amount of the driving force on the diff round that is directed sideways and onto the plates. E.g., on the power/drive side ramp, 45 degrees transmits less force sideways than 30 degrees. Likewise, on the brake/coast side ramp, an 80 degrees angle will transmit little or no force while 45 degrees does. Check to see which different side rear rings to available for each model of diff. 60°/80° is normally fitted as standard;
- 3. The pre-load with which they are assembled to start. In each diff there is a pre-load spacer that looks like one of the B plates, but thicker. Depending on diff model, it is either the first or last component assembled into the diff casing. Its thickness dictates to what degree the plates are pre-loaded / forced against each other. The pre-load is set and checked on each diff by holding one side gear still, via a dummy output shaft held in a vice, and by turning the other with a torque wrench. If the measured resistance is deemed too high, the spacer is ground down until the desired figure is achieved (usually between 5 to 20 lbs ft). The figure should be checked periodically as it tends to reduce as the diff runs, meanwhile a new A, slightly thicker spacer will allow re-setting;
- 4. The final and easiest adjustment is the re-arrangement of the contact order of the plates. The arrangement 1, with a plates succession A, B, A, B, A, has the maximum number of working friction faces and is the standard one. It gives the maximum resisting torque. The arrangement 3 has the minimum of working friction faces and gives the minimum resisting torque. By swapping from arrangement 1 to 3, the resisting torque approximately halves.

AVAILABLE RAMP ANGLES

| Power side | Brake side |
|------------|------------|
| 30° | 60° |
| 60° | 80° |
| 80° | 80° |
| 45° | 80° |
| 45° | 45° |

DIFFERENTIAL LAY-OUT

- Make sure the plate arrangement is always equal on left and right-hand side.
- Side gear ring, diff end plate, diff wall and pre-load spacer all act as "B" plates
- Bigger ramp angle transmits less thrust onto plates than smaller one.



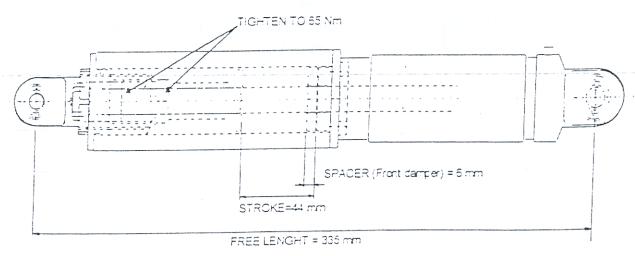
DAMPERS

DIMENSIONS & GENERAL INFORMATION

 Standard dampers are KONI 2812-140. Front and rear dampers have identical valving, the same full-extended length and identical installation parts. Damper assembly dimensions are:

| | mm |
|--------------------|-----|
| full open length | 335 |
| full closed length | |
| (front) | 297 |
| (rear) | 291 |
| stroke | |
| (front) | 38 |
| (rear) | 44 |

- The difference in stroke and full closed length is due to the 6mm Teflon spacer on front damper to prevent the rocker to lock. If you use different dampers check that max stroke is not more than 38 mm.
- The standard Koni damper has about 30kg of pre-load, due to the internal gas pressure.
- Dallara, on request, delivers installation kits for PENSKE and QUANTUM dampers. Eibach dampers can be installed using standard mountings.



FULL CLOSED LENGHT = 297 mm (Front)

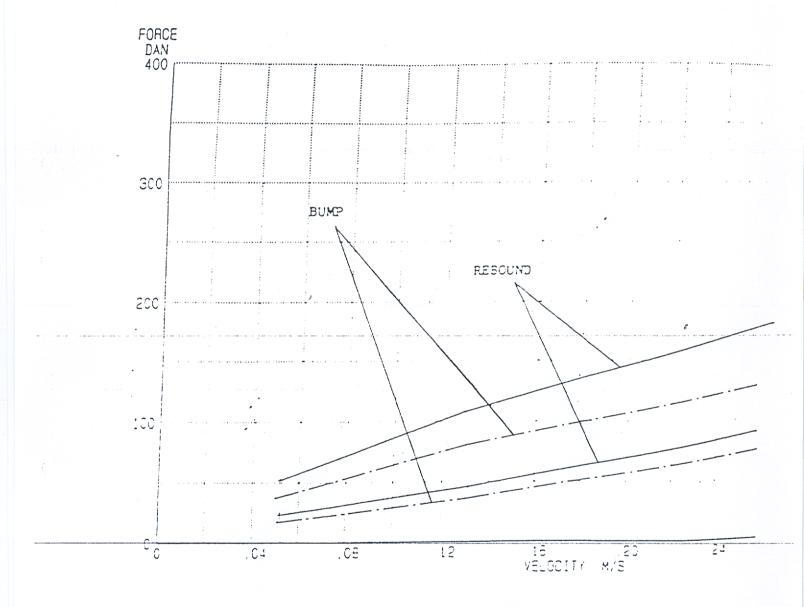
FULL CLOSED LENGHT = 291 mm (Rear)

DAMPERS DIAGRAM

The Koni dampers are adjustable both in bump and rebound by acting on the adjuster wheels marked E (for bump adjustment) and R (for rebound adjustment) on the damper top. Each adjuster wheel has eight different positions.

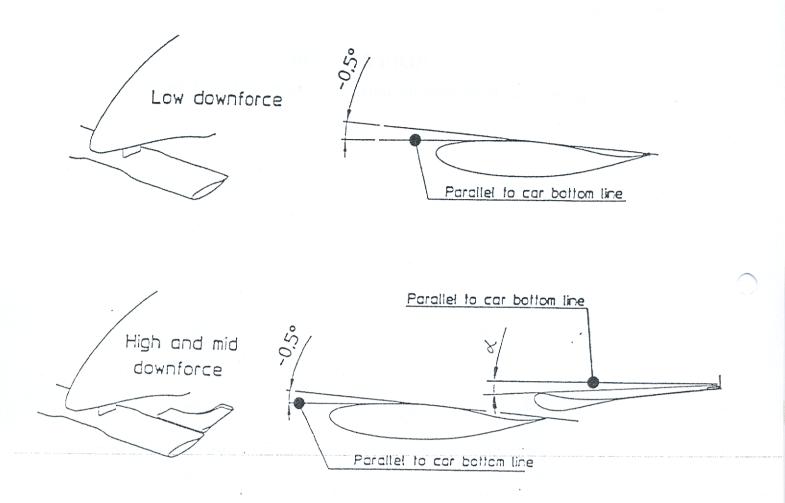
KONI 2812/140

Figure shows force/velocity graphs for full soft and full stiff settings.

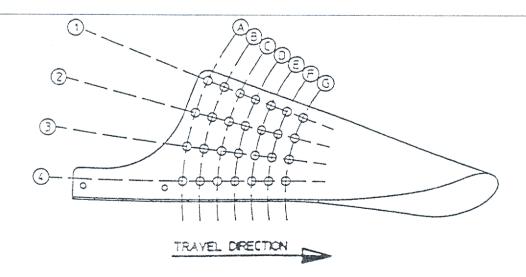


FRONT WING

FRONT WING CONFIGURATIONS



FRONT WING SIDEPLATE HOLES



REAR WING PROFILES

REAR WING

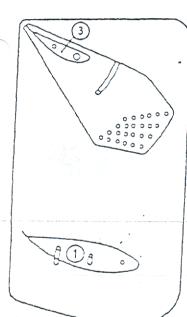




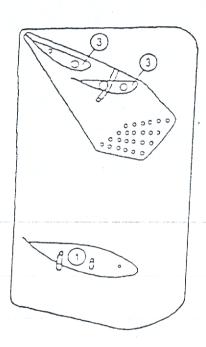


REAR WING CONFIGURATION

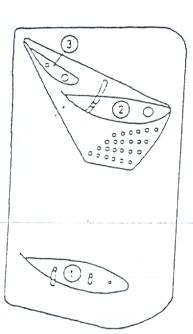
LDF LOW DOWNFORCE



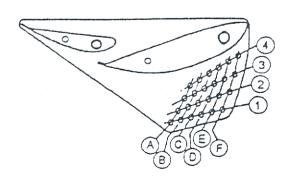
MDF MID DOWNFORCE



HDF HIGH DOWNFORCE



REAR WING SIDEPLATE HOLES



FRONT AND REAR WING SIDEPLATE TABLE

- Front flap angle is measured on top of the flap front and inside the Gurney 'corner', as shown on page 20.
- Correspondence between holes and incidence angle is just indicative, because wing angle is also function of front and rear ride heights.
- The machined side-plates allow 1 deg step adjustment.

FRONT FLAP

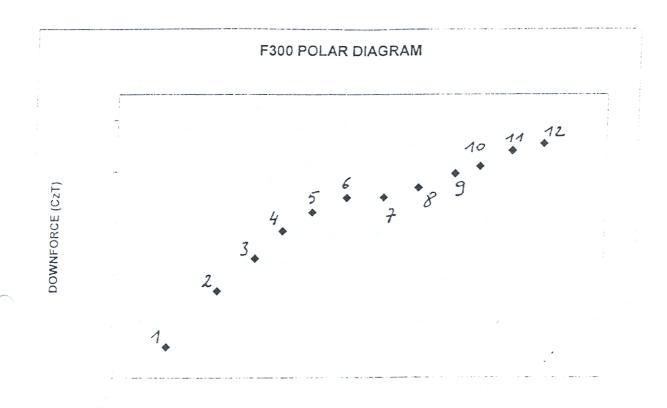
| | Α | В | С | D | E | F | G |
|---|-----|-----|-----|-----|-----|-----|-----|
| 1 | 8° | 9° | 10° | 11° | 12° | 13° | 14° |
| 2 | 15° | 16° | 17° | 18° | 19° | 20° | 21° |
| 3 | 22° | 23° | 24° | 25° | 26° | 27° | 28° |
| 4 | 29° | 30° | 31° | 32° | 33° | 34° | 35° |

REAR TOP

| | Α | В | С | D | E | F |
|---|-----|-----|-----|-----|-----|-----|
| 1 | 0° | 10 | 2° | 3° | 4° | 5° |
| 2 | 6° | 7° | 8° | 9° | 10° | 11° |
| 3 | 12° | 13° | 14° | 15° | 16° | 17° |
| 4 | 18° | 19° | 20° | 21° | 22° | 23° |

POLAR DIAGRAM

Every point corresponds to a downforce level listed below.



| REAR | FRONT |
|-------------------------------------------|---------------------------------------------|
| LDF= Low Down Force (single small top) | MF= Medium Flap (small flap) |
| MDF= Medium DF (twin small top) | SF= Standard Flap |
| HDF= High DF (small and mid combined top) | EF= Extended Flap (standard plus extension) |

DRAG (CxT)

| | REAR | REAR | | | FRONT | | | |
|-----|-------------|---------|-------|--|--------------|---------|---------------|-----|
| CFG | TOP TYPE | SETTING | LOWER | | FLAP TYPE | SETTING | MAIN PLANE | CFG |
| 1 | NONE | - | 1 | | NONE | - | -0.5 | 1 |
| 2 | LDF | 2 | 5 | | MF | 9 | -0.5 | 2 |
| 3 | MDF | 6 | 5 | | MF | 14 | -0.5 | 3 |
| 4 | MDF | 10 | 5 | | MF | 18 | -0.5 | 4 |
| 5 | MDF | 14 | 5 | | MF | 22 | -0.5 | 5 |
| 6 | MDF | 18 | 5 | | MF | 26 | -0.5 | 6 |
| 7 | HDF | 11 | 5 | | SF | 16 | -0.5 | 7 |
| 8 | HDF | 14 | 5 | | SF | 18 | -0.5 | 8 |
| 9 | HDF | 17 | 5 | | SF | 20 | -0.5 | 9 |
| 10 | HDF | 17 | 7 | | EF | 20 | -0.5 | 10 |
| 11 | HDF | 20 | 7 | | EF | 22 | -0.5 | 11 |
| 12 | HDF | 23 | 7 | | EF | 24 | -0.5 | 12 |

AERODYNAMIC information

- Front wing main-plane and rear lower wing, are set relative to the chassis reference plane.
- The optimum setting for most of the setting range is for front wing main-plane -0.5° , and for the rear lower wing $+5^{\circ}$. Any chassis rake angle will alter this setting.
- Front flap inclination is intended to be the angle, relative to the chassis reference plane, measured between front of the flap, on top and rearmost trailing edge (without any Gurney).
- Rear top wing assembly inclination is intended to be the angle, relative to the chassis reference plane, measured between front of the flap, on top and rearmost trailing edge. Any chassis rake angle will alter this setting.

Front and rear ride height settings are fundamental to the aerodynamic balance and ultimate performance of the car. Pay attention to the changes between the static setting and the dynamic values on track.

| Downforce CFG | Part | Min S Hole | Suggested Incidence | Max Sug Hole | gested Incidence |
|------------------|------|---------------|------------------------|-----------------|---------------------|
| Front | Flap | A1 | 8° | C4 | 31° |
| Rear top LDF | Wing | C1 | 0° | B2 | 5° |
| Rear top MDF/HDF | Wing | A1 | 0° | A4 / F4 | 18°/23° |

How to balance 1° FR flap variation by changing the rear wing, RR ride height?

| | | | | | 7 | |
|---------|----|-----------------------|----|-----------------------|----|------------------------|
| RR TOP→ | | LDF | | MDF | | HDF |
| | | 2 holes RR top | | 1 hole RR top | | |
| | MF | 1.5mm lower RR height | MF | 1.5mm lower RR height | | |
| | | 1mm higher FR height | | 1mm higher FR height | | 7 |
| - FD | | | • | 2 holes RR top | | 1 hole RR top |
| FR - | | | SF | 3.5mm lower RR height | SF | 2.5mm lower RR height |
| FR FLAP | | | | 2mm higher FR height | | 1.5mm higher FR height |
| | | | | | | 2 holes RR top |
| | | | | | EF | 2.5mm lower RR height |
| | | | | | | 1.5mm higher FR height |

MF: Medium Flap; SF: Standard Flap (as '99); EF: Extended Flap

COOLING ADJUSTMENT

Depending on air temperature and engine optimum water temperature you can set the cooling capacity of the radiators. Efficiency increases by sealing any eventual leakage in the inlet ducts to the radiators.

FRONT UPRIGHT

SAFETY NOTE

We advice to regularly check the **lower stud on the front uprights**, which could show little cracks difficult to detect by men's eye. Use penetrating liquid to check these studs after each accident and according the following schedule: Check after 3000km, 4000km and 5000km, after 5000km each 500km or after each race meeting or test day.

HUB ASSEMBLY

The following procedure tells to change front and rear hub bearings

· Removal of bearing

- a) Remove spigot by removing the 6 screws A;
- b) Push off drive flange by using two 6x1 screws set on thread B;
- c) Remove seeger C;
- d) Press off bearing from the upright;
- e) Push off retainer by means of two 6x1 screws set on thread B.

· Replacement of bearing

- a) Press wheel bearing into the upright;
- b) Fit seeger C;
- c) Press the retainer into the wheel bearing;
- d) Place spigot in position on the drive flange, fit A screws, washers and nuts and tighten to 41 Nm (Caution: this value is for 12K screws only).

· Wheel stud removal

- a) To reduce resistance to Loctite, heat wheel stud and retainer to 180°C;
- b) Remove pin D, remove wheel stud.

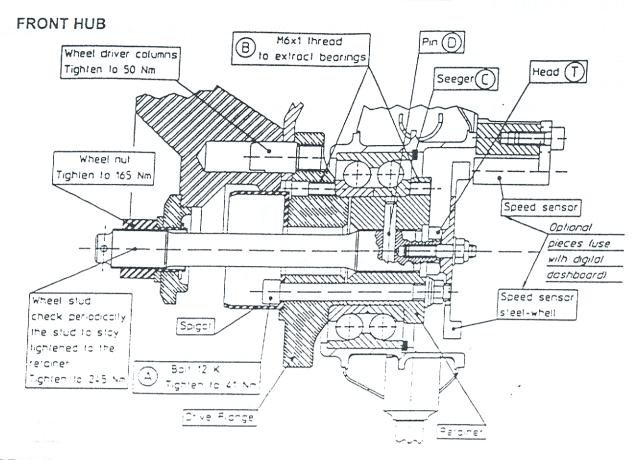
· Wheel stud replacement

- a) Remove pin D:
- b) Clean and degrease retainer thread and wheel stud;
- c) Spray degreaser to threaded area of retainer and wheel stud. Caution: Don't use petrol;
- d) Apply LOCTITE 638 to wheel stud thread;
- e) Screw wheel stud into retainer and tighten to 245 Nm by forcing on head T;
- f) Drill wheel stud and insert pin D.

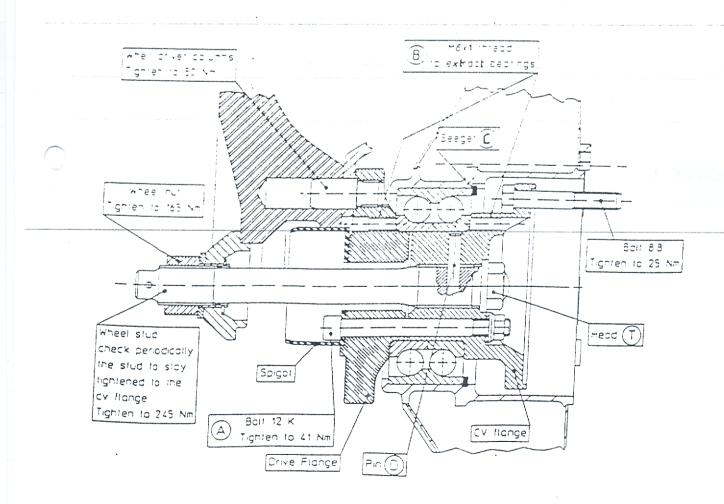
Bearing assembly into hub replacement

- a) Warm the hub to 100°C;
- b) Fit the bearing assembly

HUB ASSEMBLY



REAR HUB



SYSTEMS

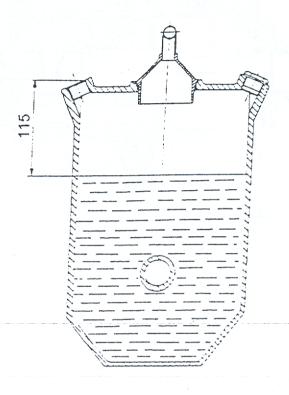
ENGINE OIL SYSTEM

We recommend keeping the oil level at 115 mm from the oil cap, measured with running engine.

Less oil may cause cavitation and so air to get into the oil circuit.

More oil may cause power loss.

Typically you would need 4.5 litres to fit in the oil tank, or 5.0 when using an oil cooler.

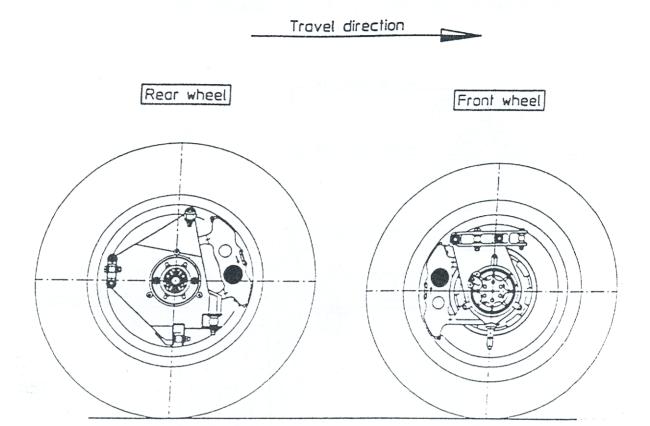


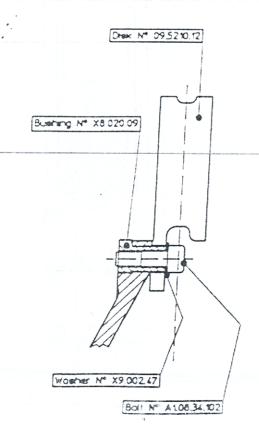
GEARBOX OIL

Typically you would need 1.2 litres to properly run the gearbox and the differential.

BRAKE SYSTEM

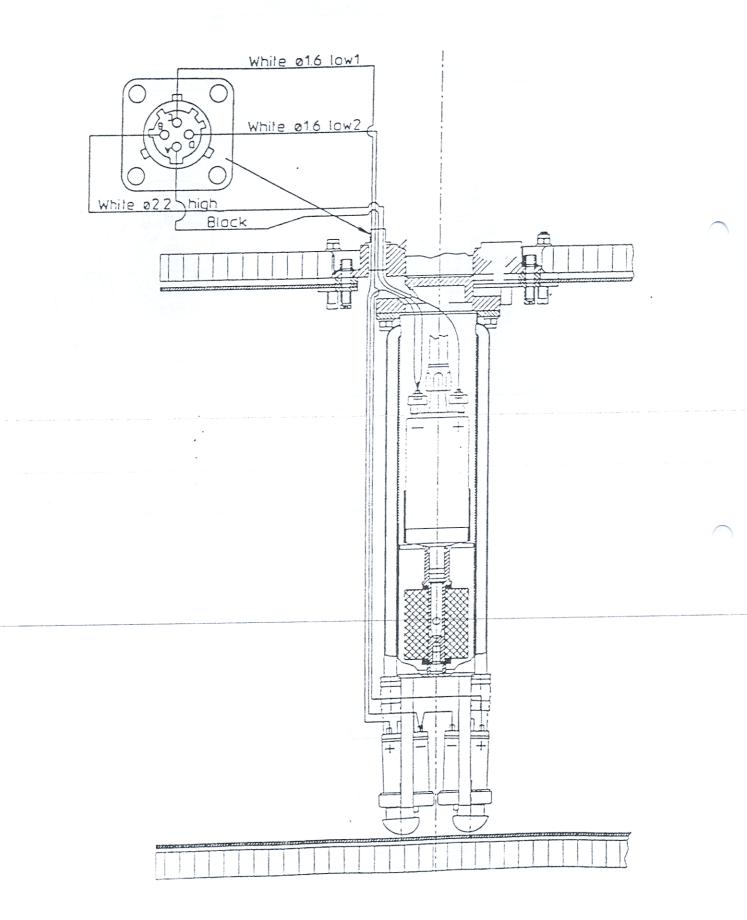
BREMBO BRAKE CALIPER ASSEMBLY





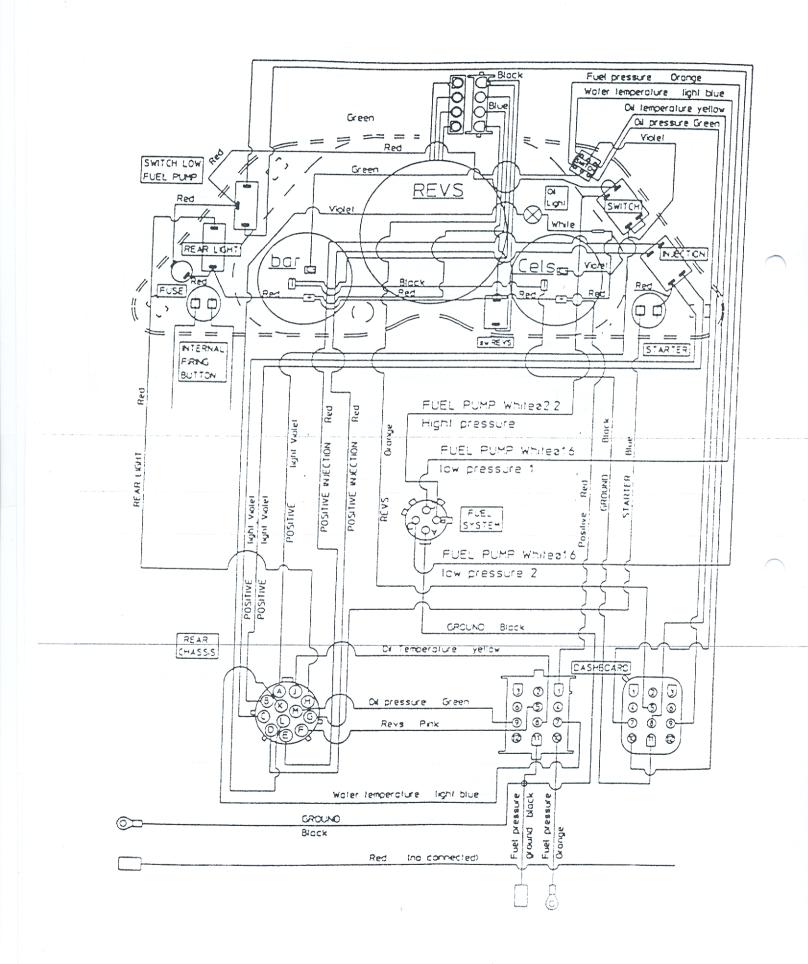
FUEL SYSTEM

- F300 features twin electrical-submerged fuel pumps as a redundant caution in case one pump fails. The driver can switch between the two pumps from the cockpit.
- OPEL-Spiess installation has a specific high-pressure pump.

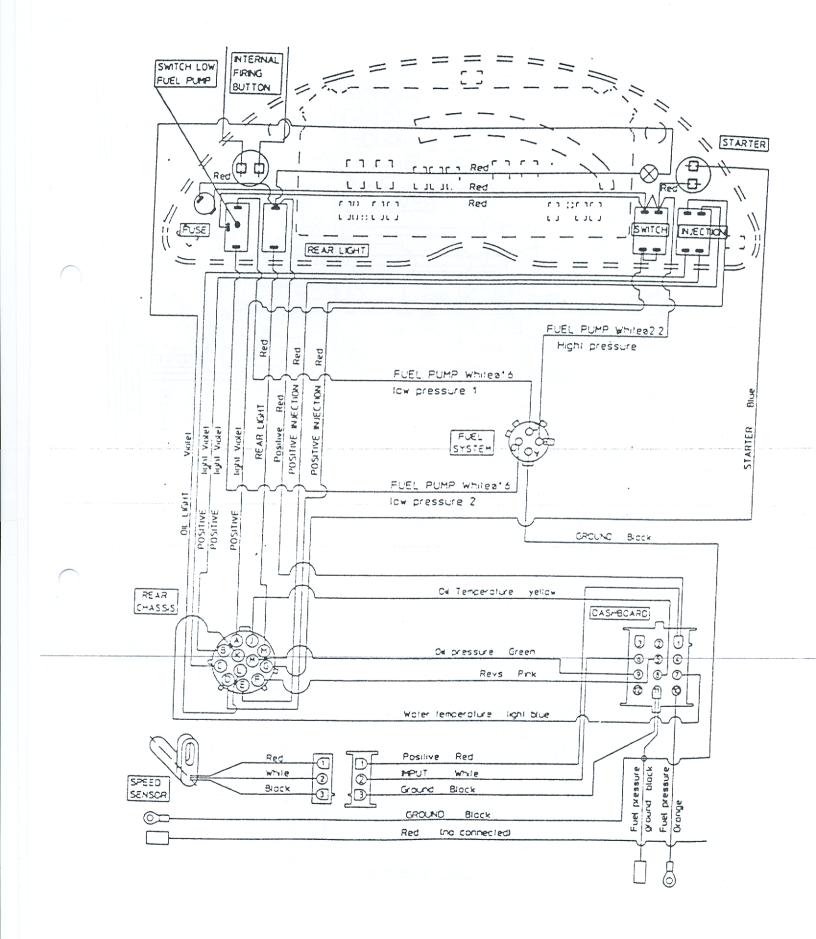


ELECTRICAL SYSTEM

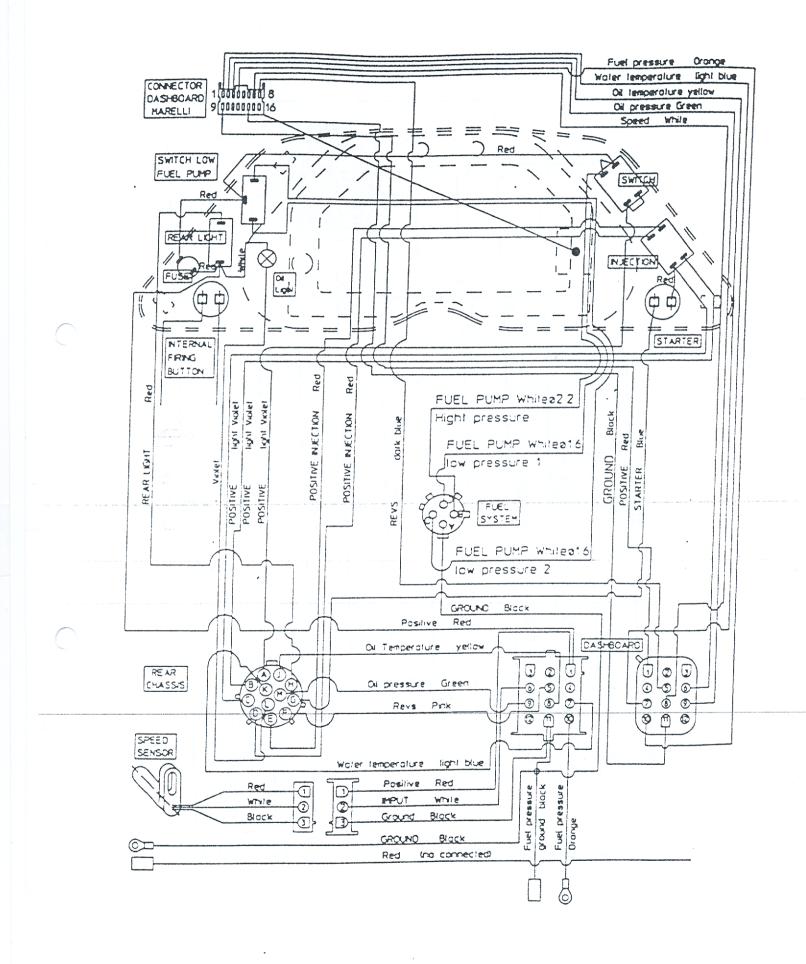
Analogical dashboard wiring



Pl and BOSCH dashboard wiring

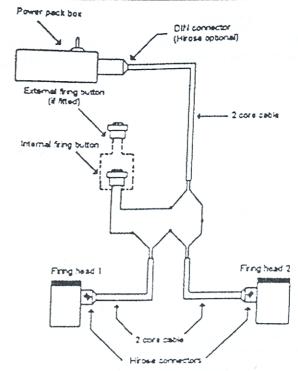


MARELLI dashboard wiring



| (-) - | OIL PRESSURE | Green | |
|--------------------|--------------------|--------------|---|
| | OIL LIGHT | Violet | |
| | WATER TEMPERATURE | Light blue | |
| | OIL TEMPERATURE | Yellow | |
| | REAR LIGHT | Red | |
| (E) — | STARTER | Blue | |
| (i) — | REVS | Pink | |
| | POSITIVE INJECTION | Red | |
| (m) — | POSITIVE INJECTION | Red | |
| (0) - | BATTERY POSITIVE | tight Violet | 7 |
| (0) - | BATTERY POSITIVE | light Violet | |
| (8) - | BATTERY POSITIVE | light Violet | |
| (D) - | | | |

EXTINGUISHER SYSTEM LAYOUT



DETAILS

The SPA Fire Fighter system is an electrically triggered Halon or foam spray fire extinguisher system. The system uses actuators to operate the valves located on the pressurised container, containing the extinguishing liquid. These are triggered remotely using a battery powered 'power pack'.

In order to guarantee reliability the actuators are of military specifications. The system/battery test electronics are integrated into the remote power pack. Connectors on the firing heads are also of military grade and use two contacts per lead to guarantee the best connections.

Actuators are designed either to operate individually, or connected in series if two heads are used.

TESTING

The power pack electronics can test the continuity of the electrical wiring, and provides a high current pulse test on the battery, to ensure system integrity before use. The battery test electronics do not excessively drain the battery during this test.

The tests are carried out using a three-way switch on the power pack. Since the system is only as good as the battery that powers it and the integrity of the wiring and its connections, the tests should be performed before each race.

To check the battery, press and hold up the power pack switch. Every 2 seconds you'll see a YELLOW light flash. If the light flashes very dimly the battery should be replaced. In doubt change the battery.

To check the wiring continuity, ensure that the power pack switch is on "SYSTEM INACTIVE" to ensure that the extinguisher is not fired. Press the internal firing button and check that the RED light comes on. Press the external firing button and check that this also makes the RED light comes on.

CARES

Ensure that the electric 'command' cables are not laying next to or in the same loom as the car battery power cables or ignition cables. Ideally, all cables should lay next to the chassis (earth);

Ensure that all plugs exposed to water spray are protected with rubber boots;

If tubing is to be removed, push orange collet in. While holding in the collet, pull out the tube; Avoid any cable to run over sharp edges without protection;

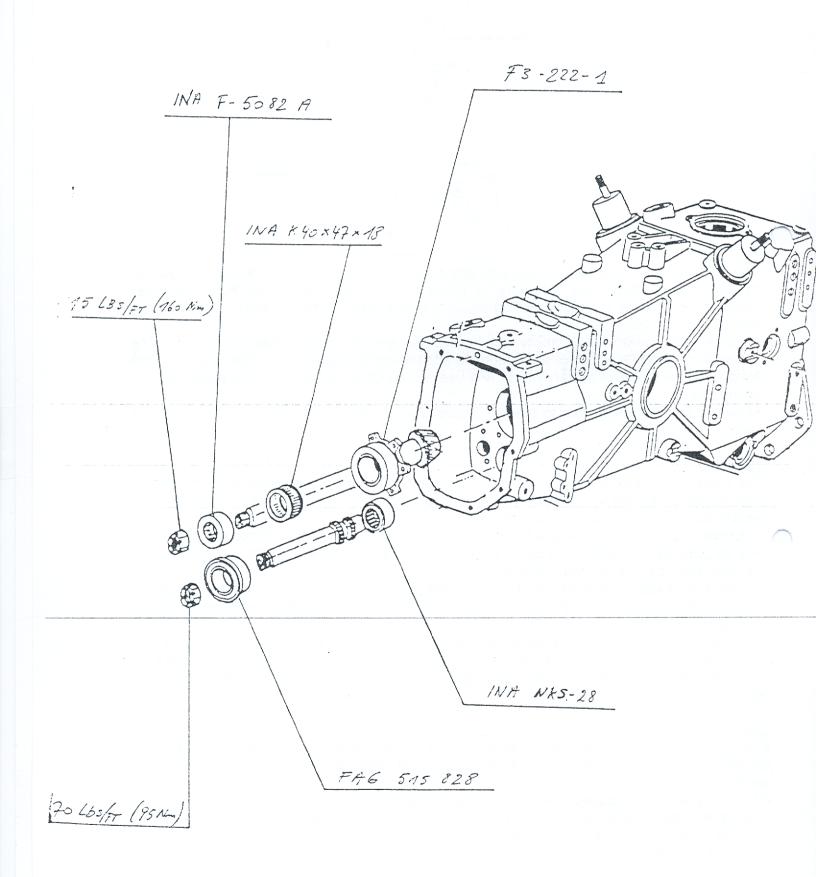
Do not fix the cables next to or onto any surface likely to exceed 200 °C;

Do not turn the firing heads when the system is activated.

GEARBOX

GEARBOX BEARINGS AND TORQUES

For ease of maintenance and replacement you find in this drawing the standard fitted bearings in the gearbox and the tightening torques we suggest for the primary and secondary shaft nuts.



SAFETY AND UTILITY NOTICES

In case of anomalies, contact immediately Dallara.

SAFETY NOTICES STUD INSTALLATION AND REMOVAL

It is very important to take an extreme care when removing and substituting the studs. Typically use:

Loctite 270 (soft Loctite)

for suspension brackets, brake calipers

Loctite 242 (hard Loctite)

for chassis, gearbox, bell-housing, roll hop

Most of these studs are loctited and do require a proper installation procedure to follow

- Clean the hole from dust, debris
- Drive a screw tap to remove machining residuals
- Clean the hole with compressed air
- Pre assemble the stud without Loctite and remove
- Clean the hole again with a degreaser and dry with compressed air
- Coat the hole with Loctite
- Install the stud
- Tight the stud with the recommended tightening torque, you can do so by using a pair of nuts locked against each other.

TRANSMISSION:

To prevent the drive-shaft bolts from loosing, fit them with LOCTITE 242;

Take good care to the fire extinguisher: F399 models have electrically operated activation with small explosive charge. Notice to all the team crew for improper handling.

It is forbidden to extract from mid downforce rear wing assembly the small profile and to use it for the rear low downforce configuration because they are differently reinforced. Buy the

When running the car with a rear ride height of 45mm or more, please, check the height of the wing endplate. Total height cannot exceed 900mm.

STEERING:

Steering rack side tie rod ends must be absolutely replaced in case of crash.

FUEL SYSTEM:

Dallara, on request, can deliver quick release adapter for the fuel line connector

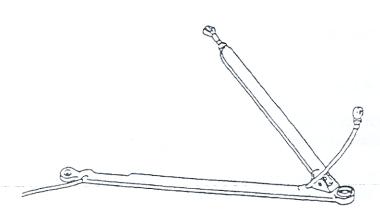
When using a thicker than F3 typical AP twin-plate metal clutch (i.e. carbon clutch...), please check that the clutch piston can move backwards enough to release the clutch completely. You can shorten the clutch piston spacer by turning off the required amount.

WISHBONES:

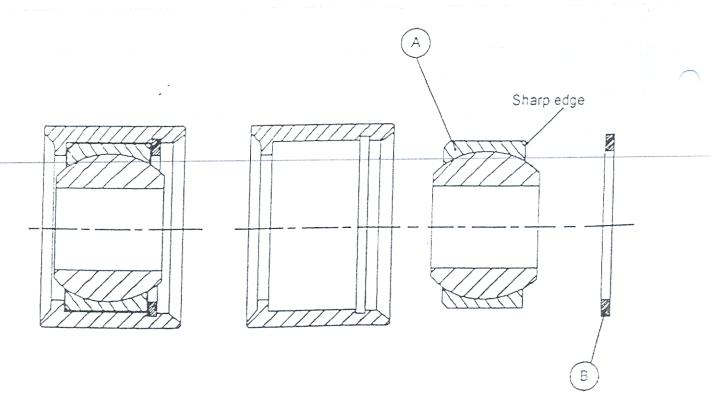
Never lift up the car, taking the middle of the wishbones. Never sit or stand on the wishbones.

SUSPENSION

- Check pin to inner hub tightening both for front and rear upright assembly. You can
 notice if the locknut came loose by observing relative displacement of two red
 notches on locknut and on spigot.
- Check every 1000 Km lower pin locknut of front hub to prevent coming loose.
- Check the front upright lower stud on cracks after 3000km, 4000km and 5000km, after 5000km check them every 500km or after each race meeting or test day.
- After any accident, check alignment of front and rear pushrod and of their respective adjusters.
- Wishbones are treated with PARCO-LUBRITE. Clean the surface with acetone before inspection.
- Check periodically the K-nuts, which fixes the blades of rear antiroll bar to the drop links: they shouldn't come loose.
- Ball joint A, used in front lower and rear lower wishbones, must be fitted with sharp side in contact with seeger B, as shown in following sketch.



Front lower wishbone



TIGHTENING TORQUES

The table lists some suggested tightening torques. For additional security use LOCTITE 242 or 243.

| | 17 | 11 64 |
|-----|-----------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Nm | Kgm | lbs ft |
| 330 | 33.5 | 250 |
| 198 | 20.2 | 150 |
| 73 | 7.5 | 55 |
| 7 | 0.7 | 5 |
| 50 | 5.1 | 38 |
| 165 | 17.0 | 125 |
| 245 | 25.0 | 185 |
| 65 | 6.6 | 49 |
| 50 | 5.1 | 38 |
| 17 | 1.7 | 13 |
| 25 | 2.5 | 19 |
| 39 | 4 | 29 |
| 34 | 3.5 | 25 |
| 54 | 5.5 | 40 |
| 3 | 0.3 | 2 |
| 15 | 1.5 | 9 |
| 30 | 3.0 | 18 |
| 45 | 4.6 | 37 |
| | 198 73 7 50 165 245 65 50 17 25 39 34 54 3 15 30 | 330 33.5 198 20.2 73 7.5 7 0.7 50 5.1 165 17.0 245 25.0 65 6.6 50 5.1 17 1.7 25 2.5 39 4 34 3.5 54 5.5 3 0.3 15 1.5 30 3.0 |

SWG & CONVERSION TABLE

This table provides conversion from SWG (Std Wire Gage) to metric units for sheet-metal thickness

| SWG | 8 | 10 | 12 | 14 | 16 | 18 | 20 |
|-------------|-------|-------|-------|-------|-------|-------|-------|
| Metric [mm] | 4.064 | 3.251 | 2.642 | 2.032 | 1.626 | 1.219 | 0.914 |

CONVERSION TABLE

| | | | | 1_ |
|----|---|---|---|----|
| Le | n | a | Ι | n |

| 2011941 | |
|---------------------------|---------------------------|
| 1 inch=25.4 mm | 1 millimeter=0.03937 in |
| 1 foot=304.8 mm=12 in | 1 centimeter=0.3937 in |
| 1 yard=914.4 mm=3 ft | 1 meter=39.37 in |
| 1 mile=5280 ft=1.60934 km | 1 kilometer=0.62137 miles |

Volume

| 1 cubic inch (c.i.)=16.387 cubic centimetres | 1 cubic centimeter=0.061 cubic inch |
|----------------------------------------------|-------------------------------------|
| | 1 liter=1000 cc=61.0255 cubic inch |

Pressure

| 1 psi=0.0716 bar | 1 kg/cm2=1.019 bar | |
|------------------|---------------------|--|
| | 1 bar=10⁵ Pa=0.1MPa | |
| | 1 bar=13.95 psi | |

Weight

| 1 ounce (oz)=28.35 grams | 1 Kg=1000 grams = 2.205 lb |
|---------------------------------------|----------------------------|
| 1 pound (lb.)=16 ounces=453.592 grams | |

Speed

| 1 MPH=1.467 feet per second | |
|-----------------------------------|----------------------------------|
| 1 mph=0.62137 kilometres per hour | 1 kilometre per hour=1.60934 mph |
| 1 IPS (in/s)=25.4 mm/s | 1 mm/s=0.039 IPS |

Specific weight

| specific weight |
|------------------------|
| Water=1 kg/l |
| Mineral Oil=0.903 Kg/l |
| Gasoline=0.74 Kg/l |

Useful formulas

| Engine displacement=0.7854 × bore × bore × stroke × no. of cylinders |
|------------------------------------------------------------------------------------|
| British horsepower (BHP)= RPM × torque (lbs ft)/5250 |
| MPH=RPM × tire diameter (in)/(gear ratio × 336) |
| $Km/h = RPM \times tire diameter (mm)/(gear ratio \times 5308)$ |
| Lap speed (MPH) =track length (miles) ×3600/lap time (seconds) |
| Lap speed (km/h) = track length (Km) × 3600/lap time (s) |
| Average speed (MPH) =track length (miles) ×3600 × no. of laps/total time (seconds) |
| Average speed (km/h) =track length (Km) ×3600 × no. of laps/total time (seconds) |

GENERAL AGREEMENT AND WARRANTY

Motor racing is not covered by warranty due to the intentional choice of drivers to race in a dangerous environment

DALLARA indicates that under normal operating conditions a new car would not show failure in structural components before it has completed around 25000 Km. This holds true if necessary maintenance and checks are provided and if the car had no previous incidents. DALLARA is not responsible for incorrect chassis repairs, if made outside its factory or in centres not recognised by FIA.

Chassis should be checked for structural failure not later than two years after delivery from DALLARA factory, and after each major accident. After first check or after any major accident it is mandatory to check the chassis every year in a centre recognised by FIA authority.

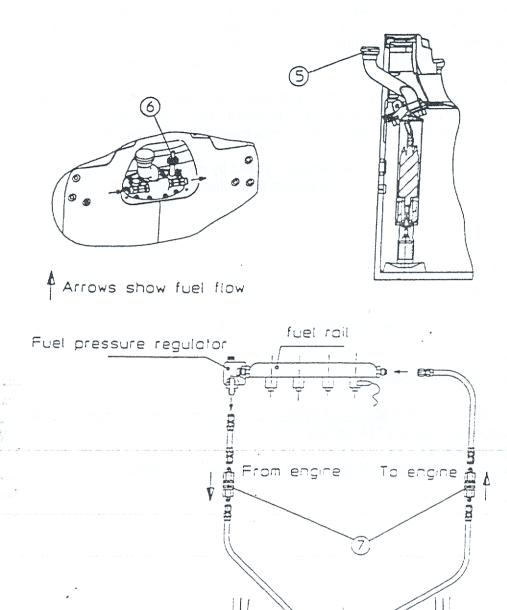
DALLARA is not responsible for damage caused by non-genuine spare parts. Under maintenance, following parts should be replaced after 25000 Km or two-years use: wiring loom;

starter motor;
steering column
steering rack and tie-rods
brake pedal;
brake disc bell;
wheel bearings;
suspension arms and spherical joints;
engine installation parts;
drive-shafts;
wings and rear wing supporting plates;

We firmly remind you that <u>Main roll over hoop</u>, <u>Monocoque</u> and <u>Front nose-box</u> (<u>crushable structure</u>) are <u>FIA approved</u> and cannot be modified by unauthorised personnel for whatever reason.

Any change to these parts is sufficient reason for disqualification.

FUEL SYSTEM LAYOUT



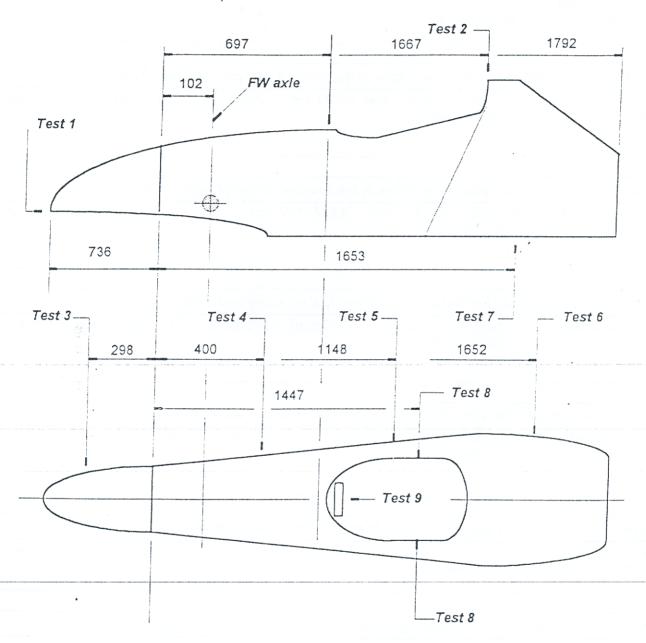
- 1) Filter
- 2) LOW pressure pump
- 3) Filter
- 4) HIGH pressure pump
- 5) Fuel cap
- 6) Breather cap
- 7) Ouick release valve also for fuel check



F3 STRUCTURE TESTING RECORD

Constructor: DALLARA Chassis type: F399 LWB
Date: 15/07/1999 Place: Dallara factory

Present : G Dallara, J. Bauer



Test 3: A 20.00kN load applied to the the nose side 40cm in front of the front axle line and held for 30 secs

Load 20.02 kN

Comments: OK., no visible damage on nose and fixation

Test 4 : A 20.00kN load applied in 3 mins to the footwell side and held for 30 secs

Load 20.00 kN Displacement 0.63 mm (mm) Difference 100 % Deformation 0.05 mm

Comments: CK., no visible damage

Chassis number: F399 - 001

Test 2: A 51.75kN load applied at a compound angle to the top of the main roll structure

Load 52.73 kN Displacement 8.90 mm

Comments: Test carried out with reference weight of 570 kg instead of 560 kg, ok. no visible damage

Test 3: A 20.00kN load applied to the the nose side 40cm in front of the front axle line and held for 30 secs

Load 20.02 kN

Comments: OK., no visible damage

Test 4: A 20.00kN load applied in 3 mins to the footwell side and held for 30 secs

Load 20.08 kN Displacement 0.55 mm (0.43 mm) Difference 100 % Deformation 0 mm

Comments: OK., no visible damage

Test 5 : A 20.00kN load applied in 3 mins in the seat belt area and held for 30 secs

Load 20.07 kN Displacement 4.37 mm 16 kN:3.54 mm Deformation 0.06 mm

Comments: OK., no visible damage

Test 6: A 20.00kN load applied in 3 mins to the fuel tank side and held for 30 secs

Load 20.02 kN Displacement 1.00 mm (0.79 mm) Difference 100 % Deformation 0.05 mm

Comments: OK., no visible damage

Test 7: A 10.00kN load applied in 3 mins to the fuel tank floor and held for 30 secs

Load 10.02 kN Displacement 3.80 mm (3.10 mm) Difference 100 % Deformation 0 mm

Comments: OK., no visible damage

Test 8: A 10.00kN load applied in 3 mins to the cockpit rims and held for 30 secs

Load 10.07 kN Displacement 0.64 mm (0.50 mm) Difference 100 % Deformation 0 mm

Comments: OK., no visible damage

Test 9: An impact test on the steering assembly at 7 metres/sec with a total mass of 8kg

1. Impact speed: 7.15 m/s Deformation: 33 mm 2. Impact speed: 7.11 m/s Deformation: 35 mm

1. Deceleration : Peak: 147.3 g Time greater 80 g: 1.1 ms

2. Deceleration: Peak: 277.9 g Time greater 80 g: 1.65 ms

Structure fixings: 2 x M6 bolts on bearing, on rack

Component weights: front part of the steering column: 665 g, collapsable part: 6 g, steering wheel: 680 g

Comments : test 1 carried out with centre pad on steering wheel, test 2 carried out without pad on

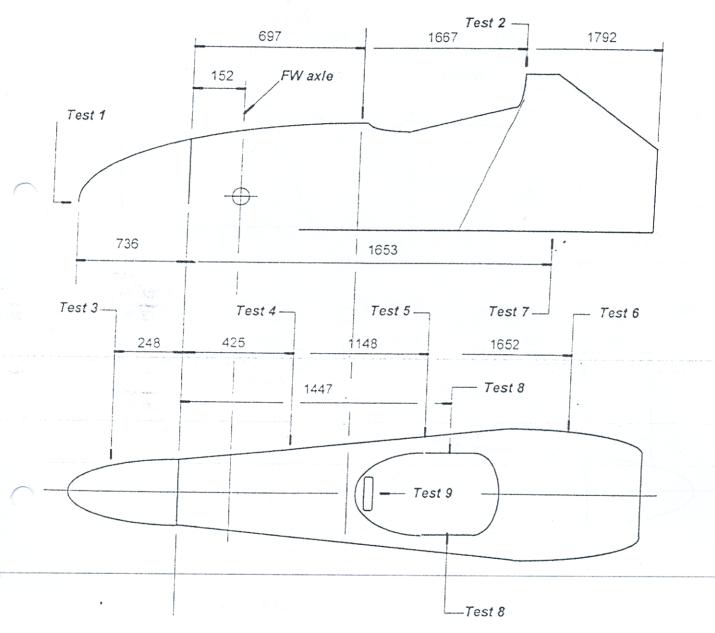
steering wheel, quick release mechanism still working after both tests, both tests OK.



F3 STRUCTURE TESTING RECORD

Constructor: DALLARA Chassis type: F399 Chassis number: F399-001
Date: 19/10/98, 16/12/99 Place: Politechnico Milan, Dallara factory, CSI

Present : Prof. Caprile, M. Anghileri, H. Gutman, A. Toso, J. Bauer



| Impact speed | : | 1st 10.1 | | Deformation | on: 1st 366 m i | n | | | |
|----------------|---|----------|----------------------|---------------|------------------------------------|----|-----------------------------------------|-----|---|
| | | 2nd 10. | | | 2nd 426 mi | η | | | |
| Deceleration | : | Peak: | 1st 20.9 2nd 19.2 | | n:14.15 g 12.17 g | | | | |
| Nose fixings | : | 4 bolts, | 8 mm diam | | Nose weight | | 1st 4.1 kg 2nd 3.03 kg | | |
| Chassis weight | : | 39.77 | kg | First chassis | : 39.77 | kg | Difference | 100 | % |

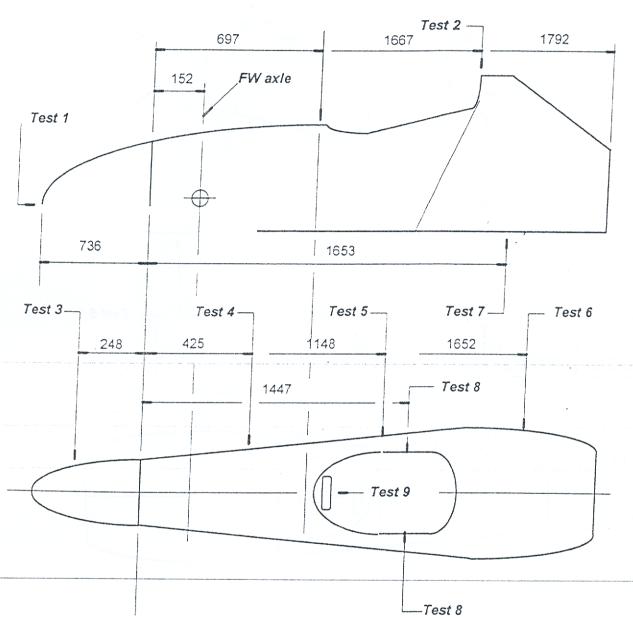
Domments



F3 STRUCTURE TESTING RECORD

Constructor : DALLARA Chassis type : F399

Date : 31/08/1999 Place : Dallara factory
Present : G. P. Dallara, J. Claes, K. H. Stegner, J. Bauer



| 51.95 K | | mm | 100% | G = 560 kg |
|----------|----------------------|----------------------------------------------------------|----------------------------------------------------------------|-----------------------------------------------------------------------|
| | 210510001110111 0.10 | mm | 110% | G = 616 kg |
| | | mm | 120% | G = 672 kg |
| 67.30 ki | N Displacement 8.90 | mm | 130% | G = 728 kg |
| | 58.00 k. 62.10 k. | 58.00 kN Displacement 6.40 62.10 kN Displacement 7.15 | 58.00 kN Displacement 6.40 mm 62.10 kN Displacement 7.15 mm | 58.00 kN Displacement 6.40 mm 110% 62.10 kN Displacement 7.15 mm 120% |